

A Wideband Dipole Array for Directed Energy Applications and Digital TV Reception

**F. Scirè Scappuzzo¹, D. D. Harty², B. Janice²,
H. Steyskal³, and S. N. Makarov²**

¹ Physical Sciences Inc., Andover, MA, USA

² Worcester Polytechnic Institute, Worcester, MA, USA

³ Consultant, Concord, MA, USA

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- **Problem and motivation**
- **The “ribcage” dipole antenna**
- **Comparisons with classic configurations**
- **Ribcage dipole antenna for communications**
 - Optimized ribcage dipole with balun
 - Simulations and laboratory measurements
- **Antenna array for Directed Energy applications**
 - Optimized unit cell with balun
 - Customized power dividers
 - 8x8 array of ribcages: simulations and preliminary laboratory tests
 - Composite array model for antenna array pattern modeling
- **Conclusions and future work**



Compact High Performance RF Communications

Motivation #1

Whip antennas for HF communications

- Simple classic design
- Narrow bandwidth
- High visibility
- Needs assembly for portability

Ribcage dipole antenna

- Low profile
- Excellent performance over a ground plane
- Wide impedance bandwidth
- Uniform antenna pattern over the bandwidth
- Needs further development and funds

Compact Portable Focused Beam Antenna

Motivation #2

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Parabolic dish antennas

- Wide band
- High gain
- Focused beam
- Simple feeding
- Complex position control
- Large volume
- Not easily portable
- Highly visible

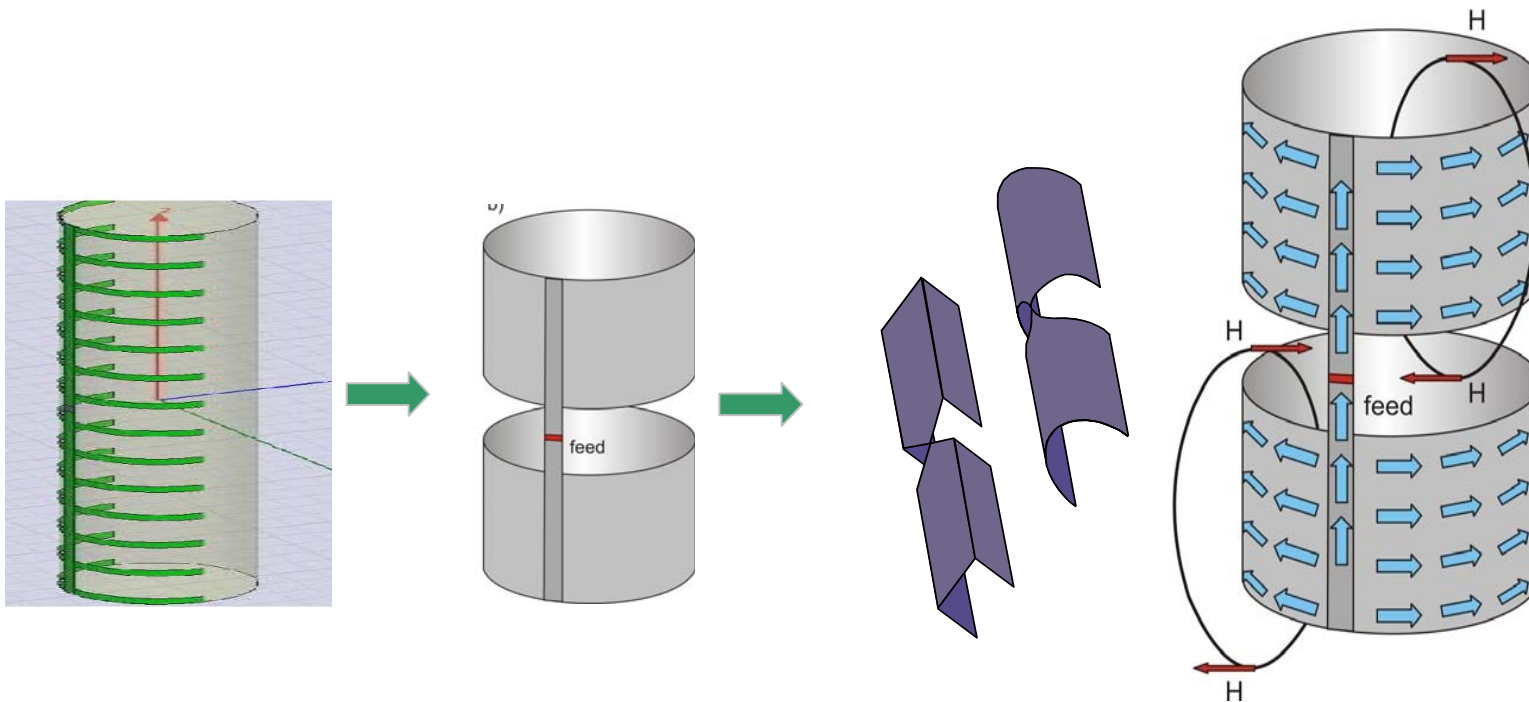
Antenna array of ribcage elements

- Wide-band, high gain, narrow beam
- Possibility of electronic scanning
- Compact, low-profile, easily portable
- Can be stowed in sub-array modules
- More complex feeding network

The Origins of the “Ribcage” Dipole

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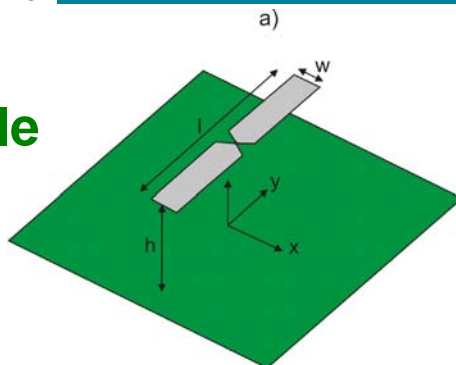
- Volumetric dipole antenna with ribs, wings, or sleeves
- Closed ring or open sleeve
- Intrinsic additional magnetic field



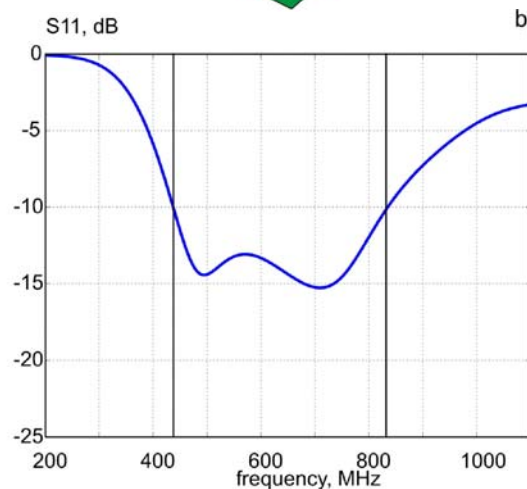
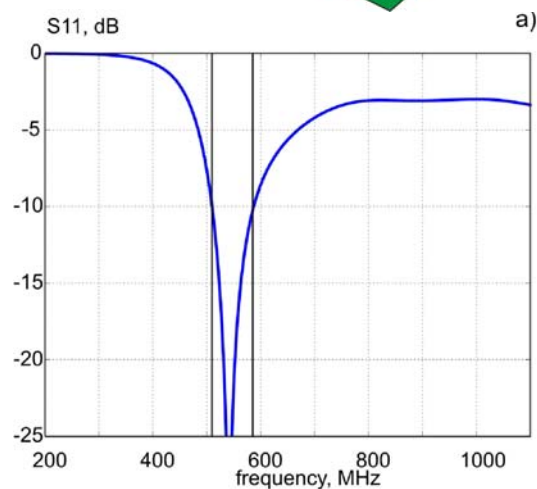
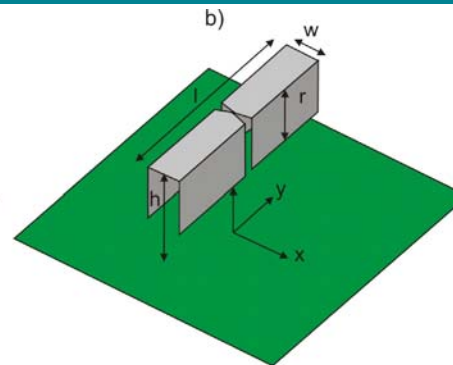
Wideband Volumetric Antenna: Dipole With Sleeves

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Blade Dipole



Ribcage Dipole



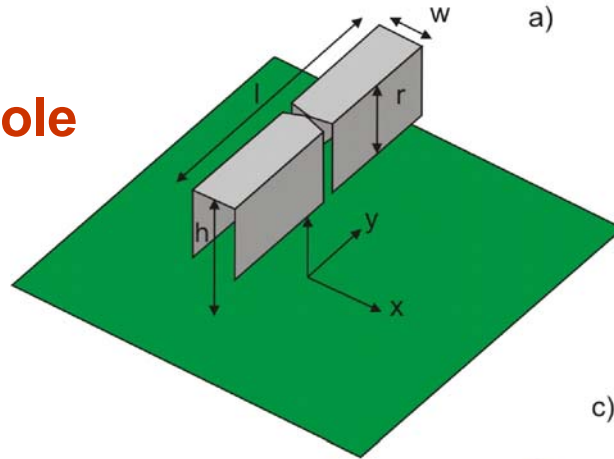
The **ribcage dipole** has wider bandwidth than **blade dipole** of same width and length.

Antenna	Height above Ground Plane	Width	Total Length	(Sleeve) Depth	Ground Plane
Blade dipole	$h=105$ mm	$w=30$ mm	$l=220$ mm	NA	300×300 mm
Ribcage dipole	$h=160$ mm	$w=30$ mm	$l=220$ mm	$r = 70$ mm	300×300 mm

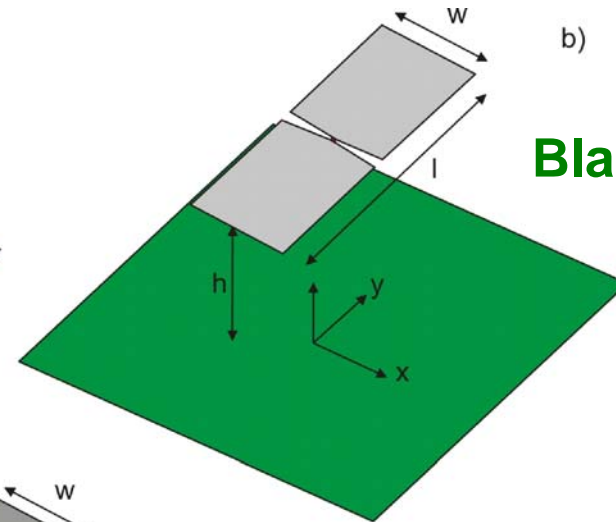
Comparison of Dipoles Over Ground Plane

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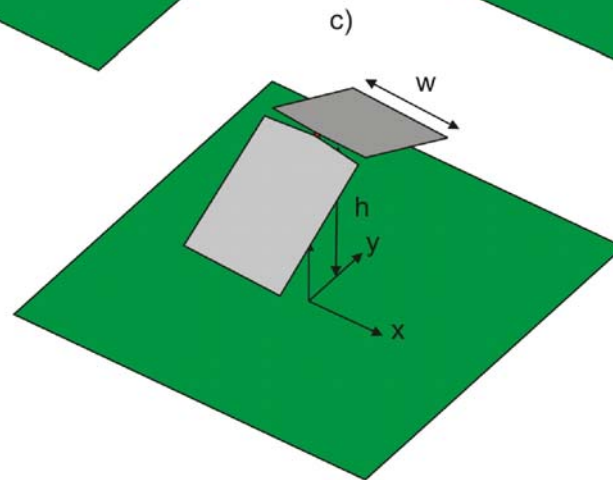
Ribcage Dipole



Blade Dipole



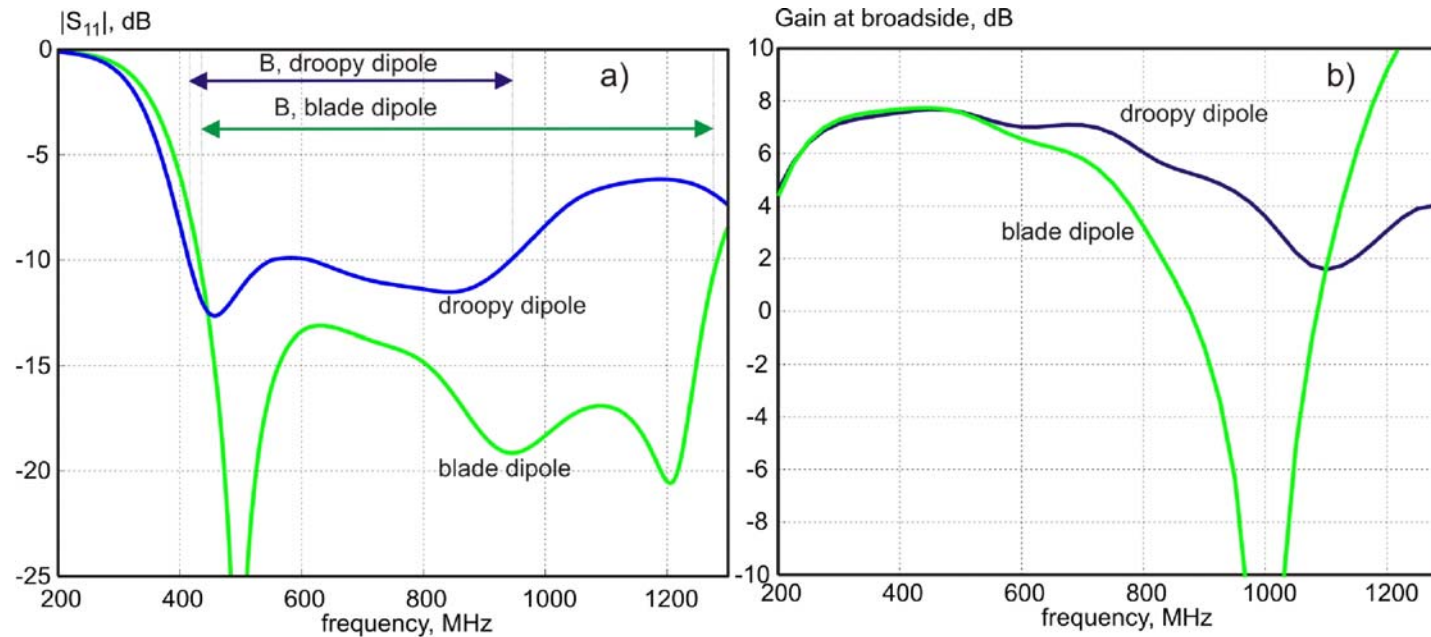
Droopy Dipole



Optimized Droopy Dipole and Blade Dipole

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Antenna	Height over Ground Plane	Width	Total Length	Sleeve Depth	GP
Blade dipole	$h=150$ mm	$w=120$ mm	$l=220$ mm	NA	300×300 mm
Droopy dipole	$h=150$ mm	$w=140$ mm	$l=220$ mm	NA	300×300 mm

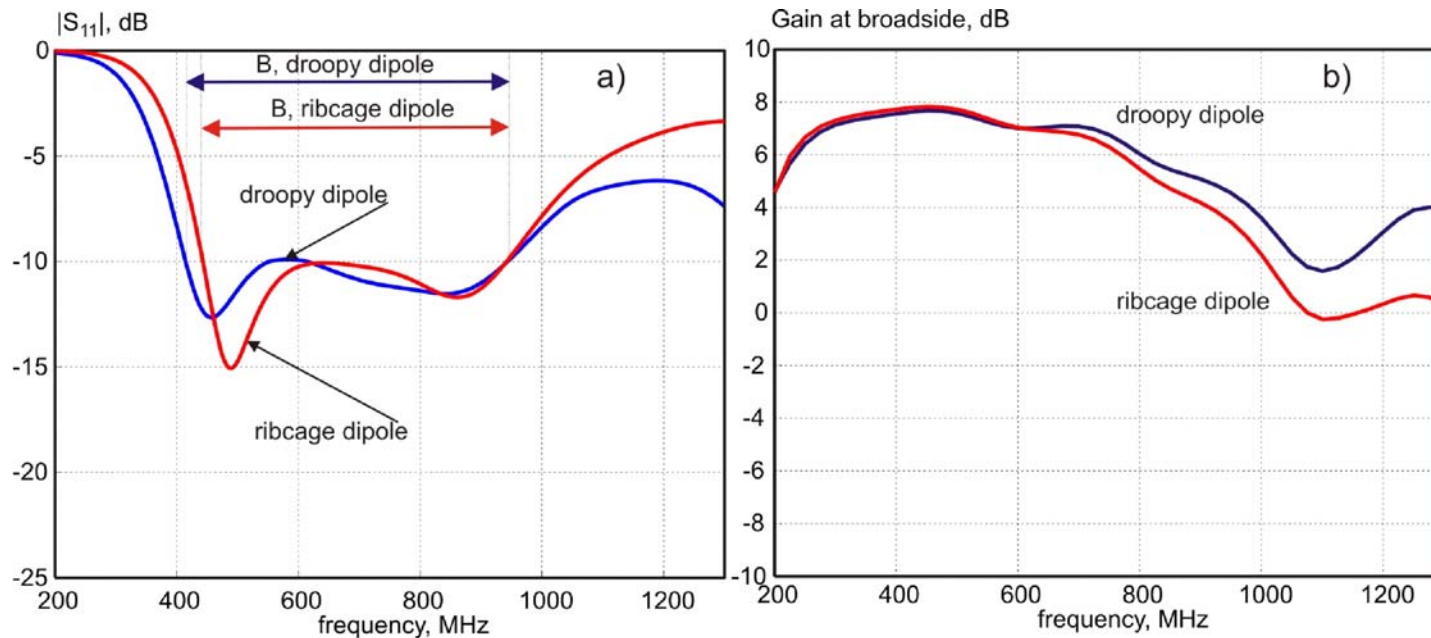


- The **blade dipole** has a wider impedance bandwidth
- The **droopy dipole** has a more uniform gain over the bandwidth

Ribcage Dipole and Droopy Dipole

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Antenna	Height from Ground Plane	Width	Length	Sleeve Depth	GP
Ribcage dipole	$h=150$ mm	$w=25$ mm	$l=220$ mm	60mm	300×300 mm
Droopy dipole	$h=150$ mm	$w=140$ mm	$l=220$ mm	NA	300×300 mm



- The **ribcage dipole** can be designed to have similar performance than the **droopy dipole**

Ribcage Dipole:

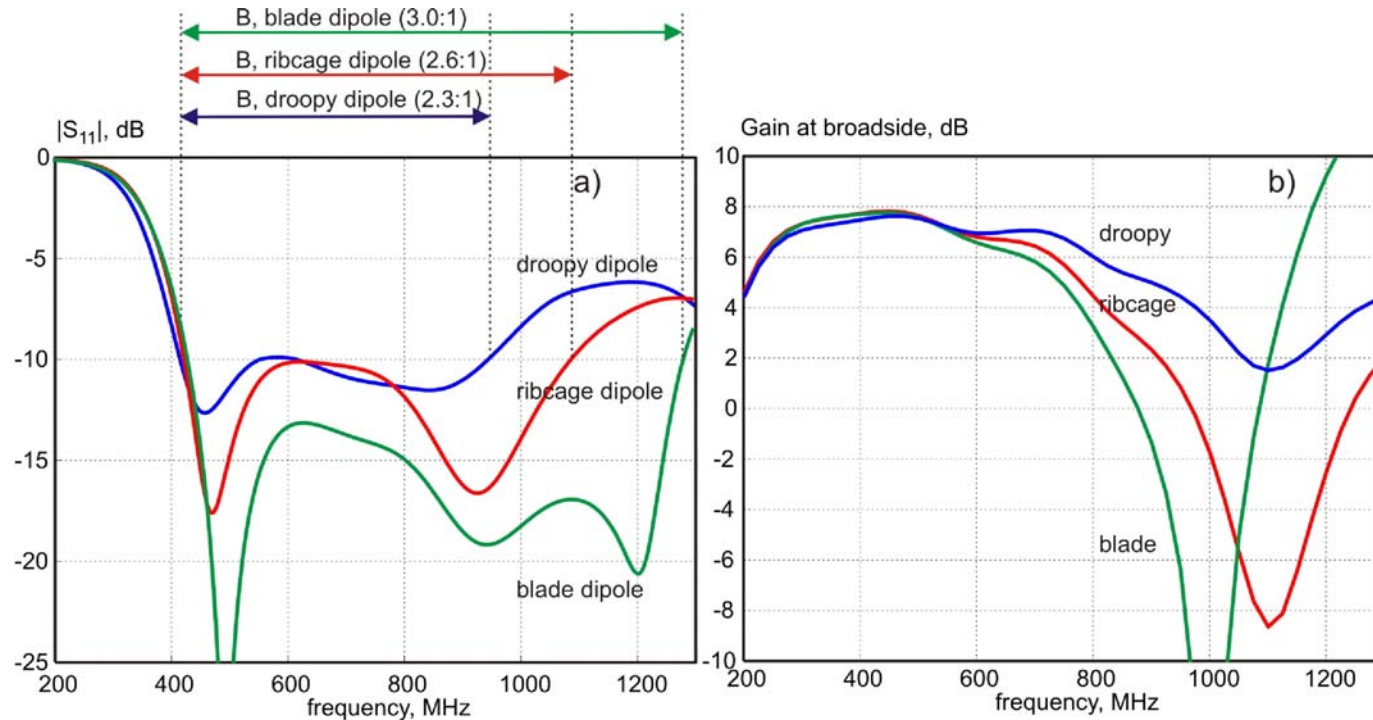


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Between Droopy Dipole and Blade Dipole

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Antenna	Height From Ground Plane	Width	Length	Sleeve Depth	GP
Ribcage dipole	$h=150$ mm	$w=55$ mm	$l=220$ mm	40 mm	300×300 mm
Droopy dipole	$h=150$ mm	$w=140$ mm	$l=220$ mm	NA	300×300 mm
Blade dipole	$h=150$ mm	$w=120$ mm	$l=220$ mm	NA	300×300 mm

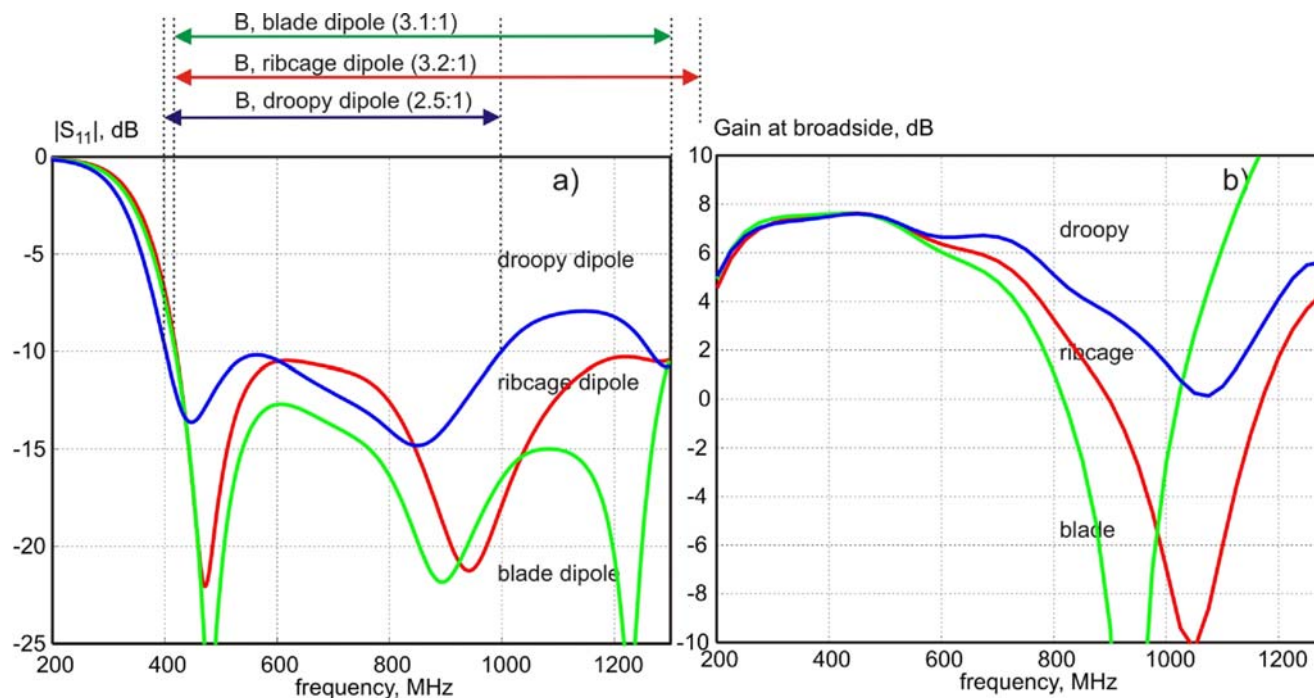


- The **ribcage dipole** can be designed to combine advantages of both **droopy dipole** and **blade dipole** (its extreme cases).

Optimized Ribcage Dipole

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Antenna	Height from Ground Plane	Width	Length	Sleeve Depth	GP
Ribcage dipole	$h=160\text{mm}$	$w=50\text{mm}$	$l=220\text{mm}$	40mm	$300\times 300\text{mm}$
Droopy-blade dipole	$h=160\text{mm}$	$w=140\text{mm}$	$l=220\text{mm}$	NA	$300\times 300\text{mm}$
Wide-Blade dipole	$h=160\text{mm}$	$w=120\text{mm}$	$l=220\text{mm}$	NA	$300\times 300\text{mm}$

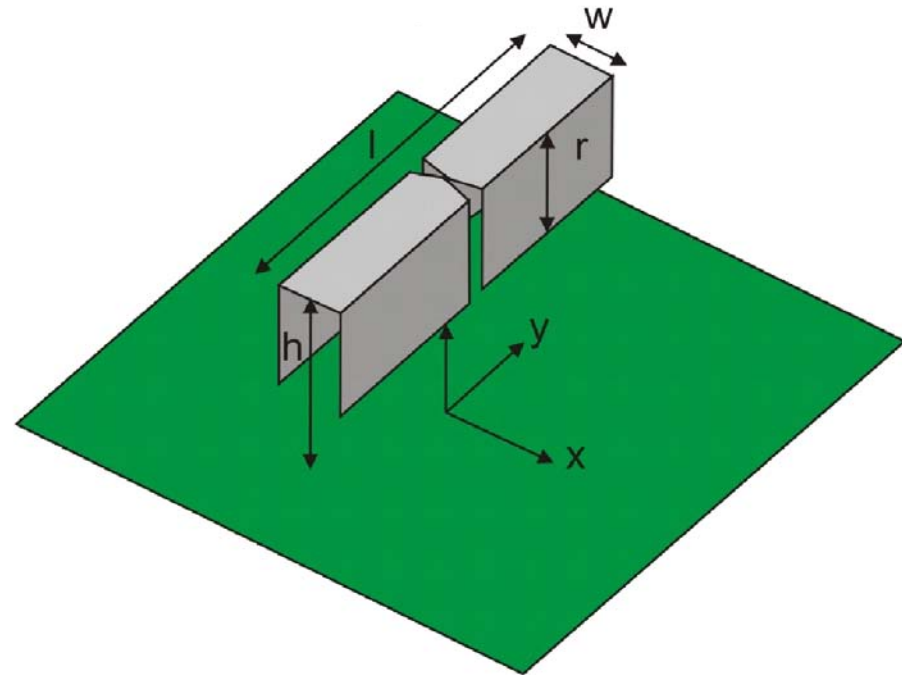


- A **ribcage dipole** can be optimized to have wider impedance bandwidth than a **droopy dipole** and better gain bandwidth than a **blade dipole**

Advantages of Ribcage Dipoles

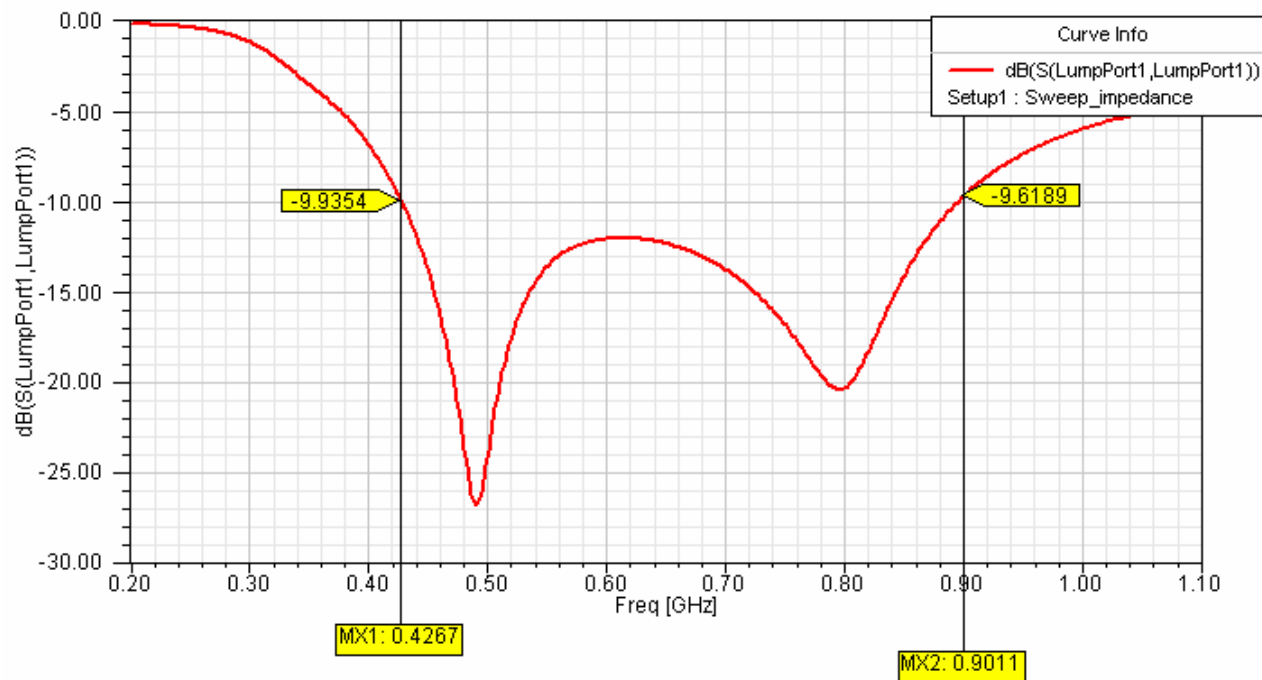
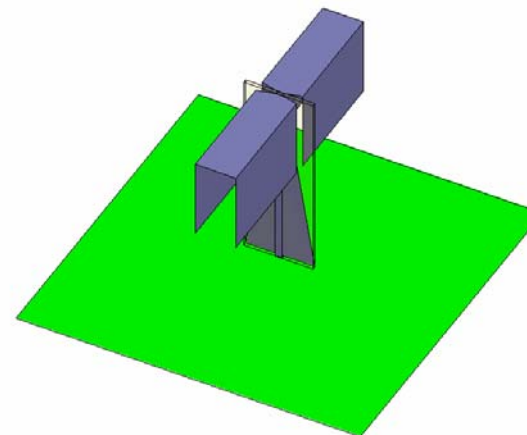
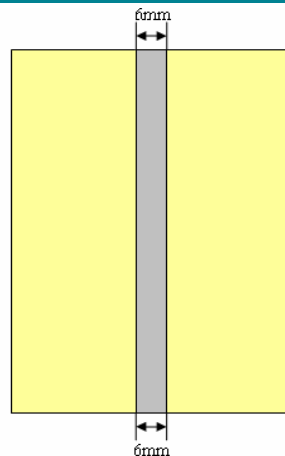
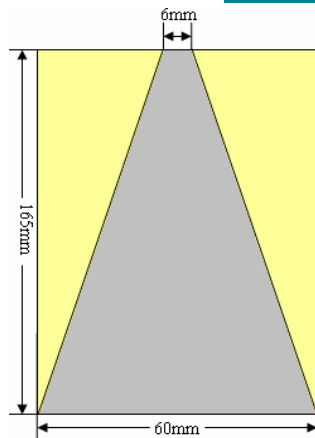
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- Space optimization
- Design flexibility (more parameters)
- Wide impedance bandwidth
- Wide gain bandwidth



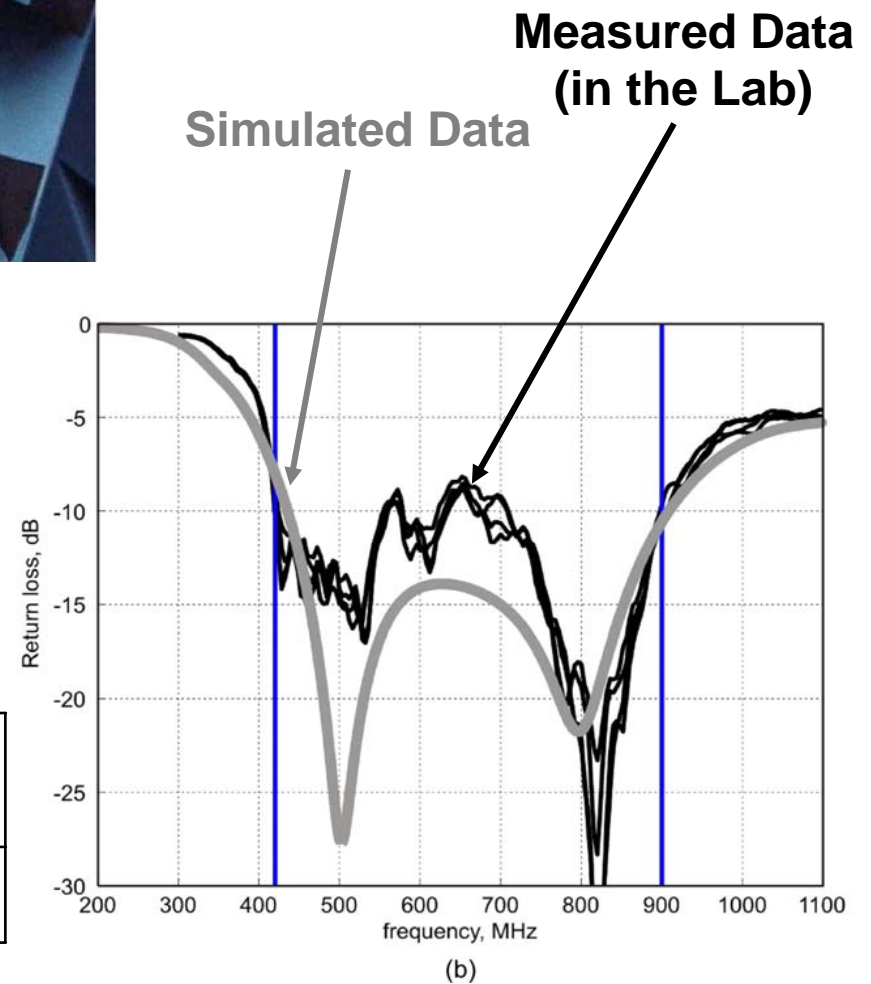
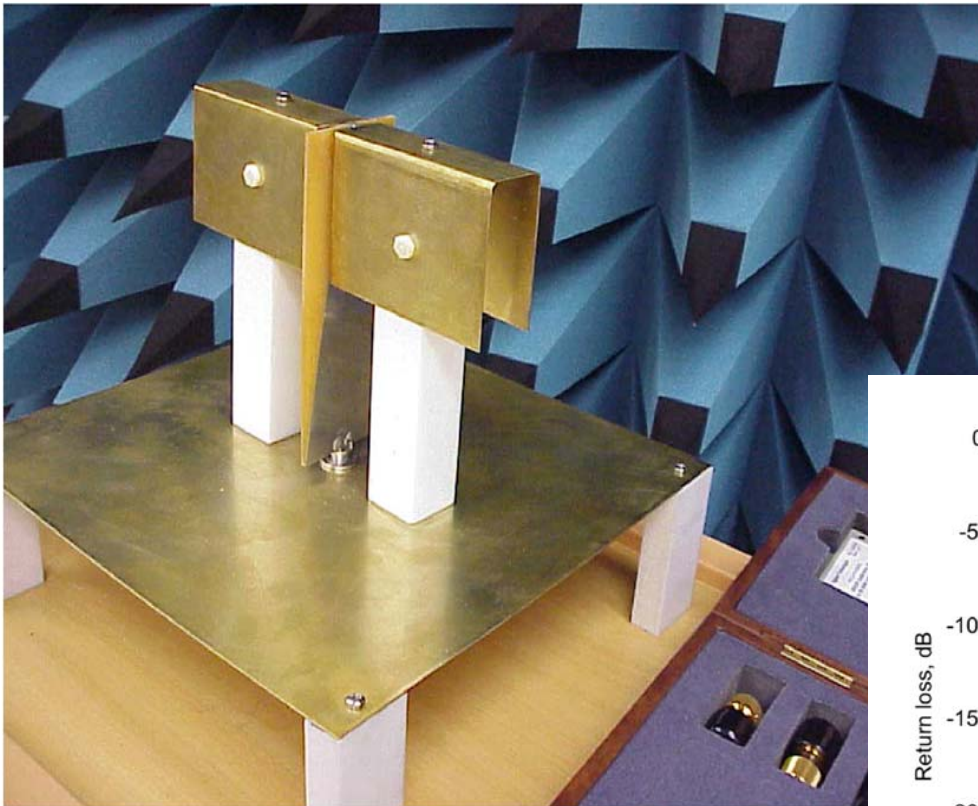
Ribcage Antenna With Tapered Balun

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Ribcage Antenna With Balun and Teflon Support

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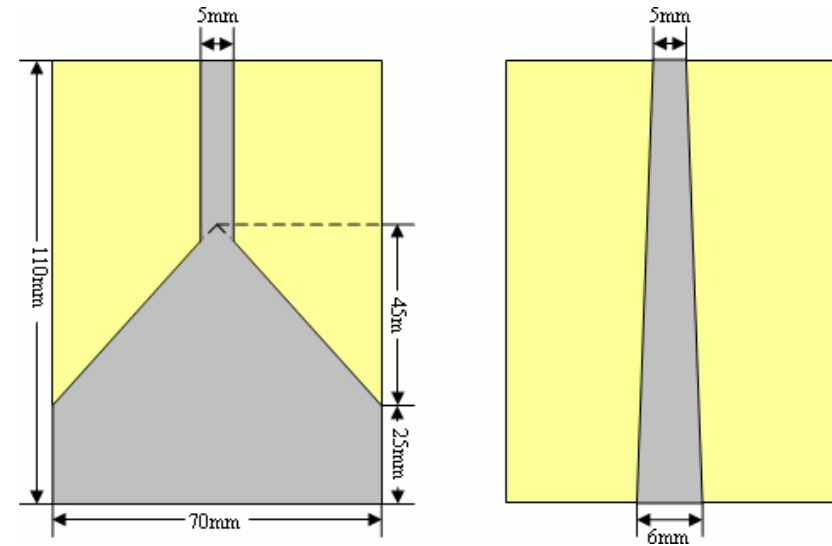
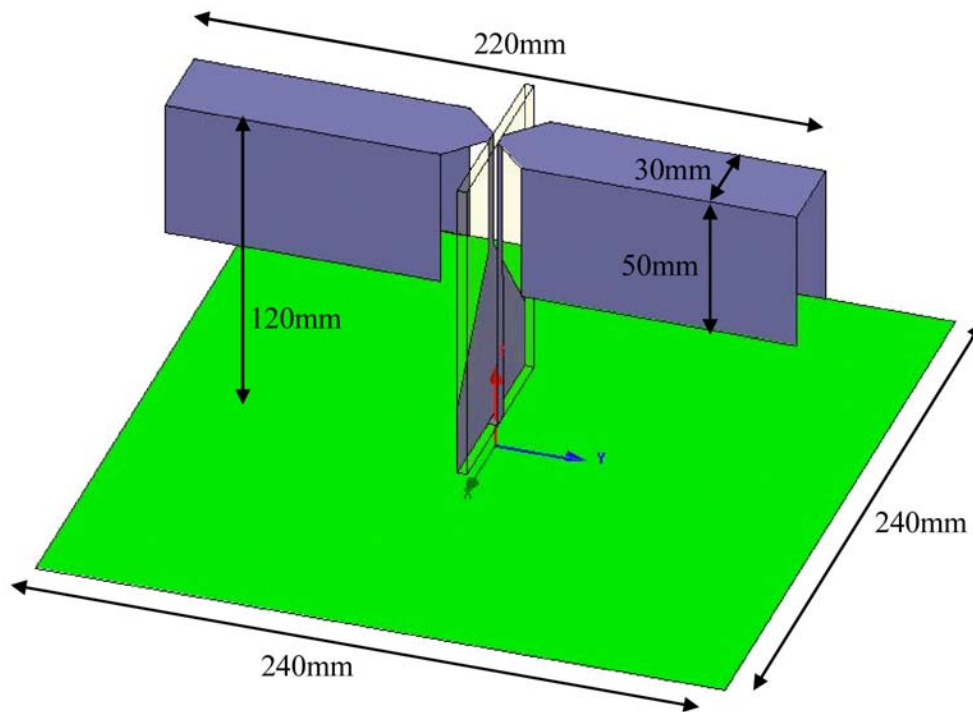


Height from Ground Plane	Width	Total Length	Sleeve Depth	GP
$h=175$ mm	$w=35$ mm	$L=210$ mm	$r=70$ mm	300×300 mm

Optimized Unit Cell With Balun

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- Optimized single radiating element for the array

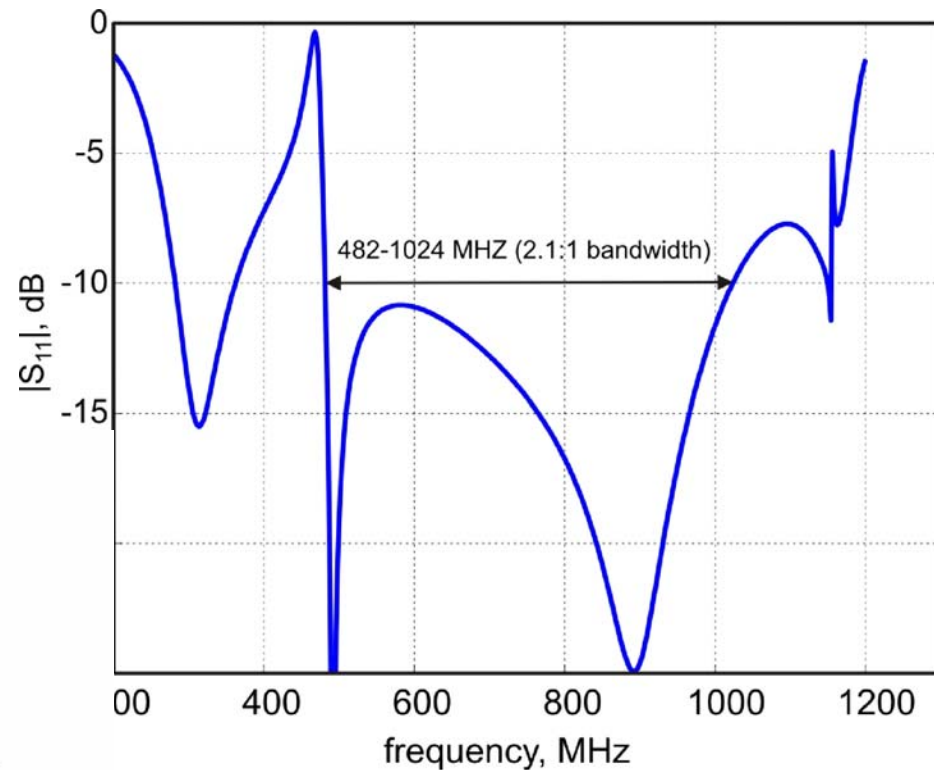
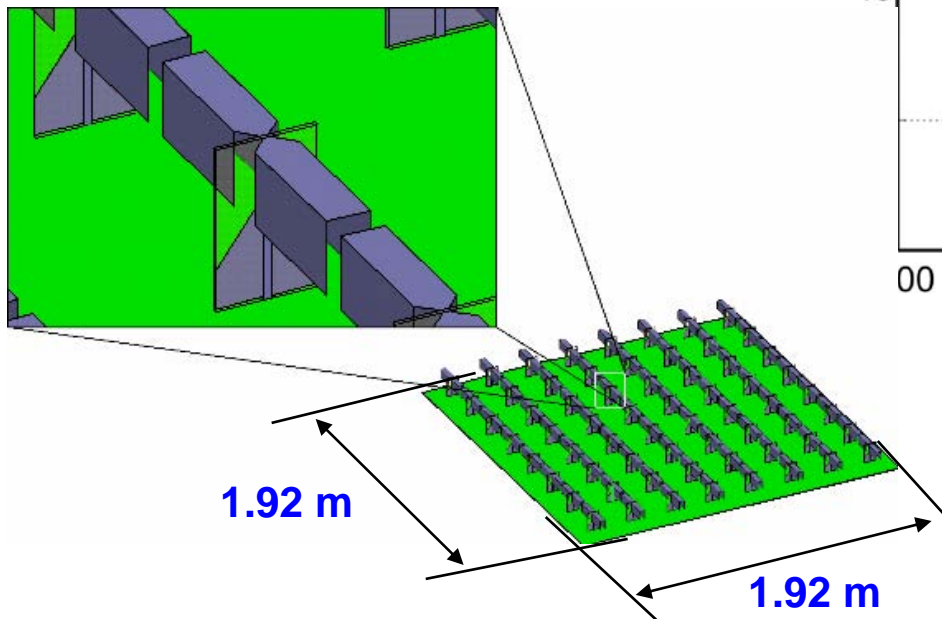


- Optimized tapered balun for the array configuration

Simulated Antenna Array Return Loss

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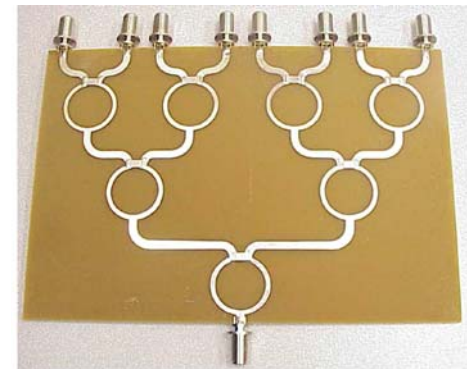
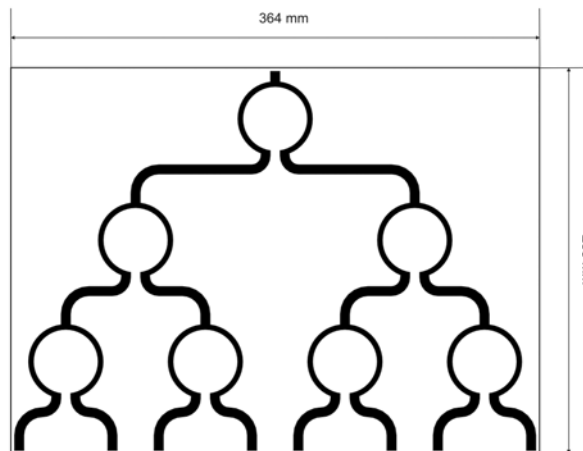
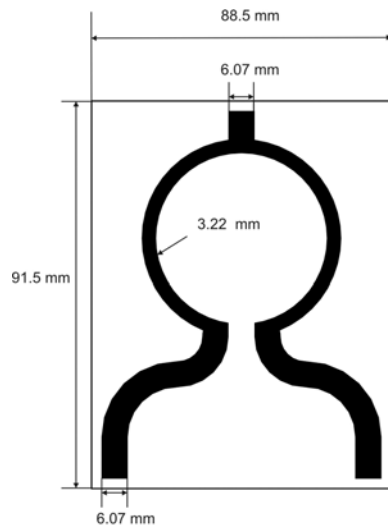
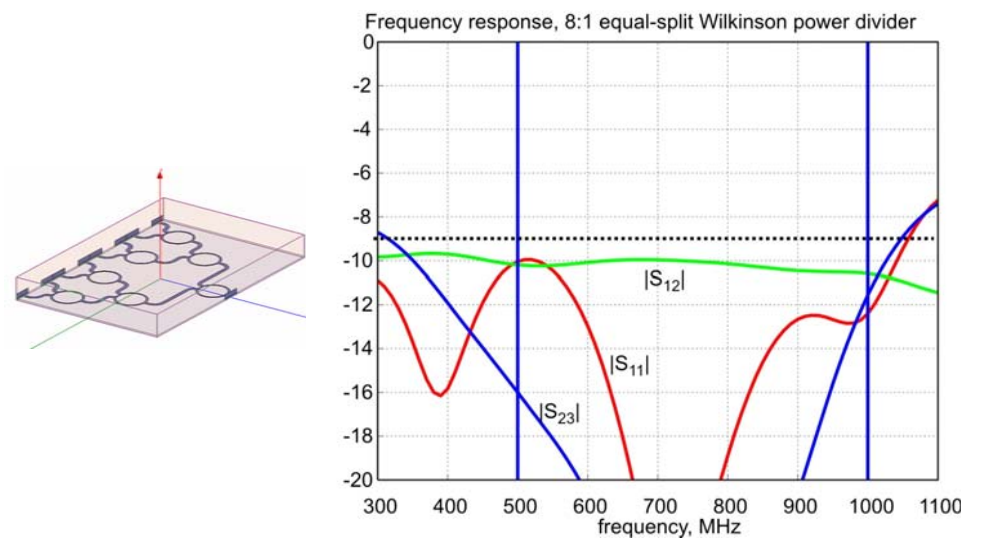
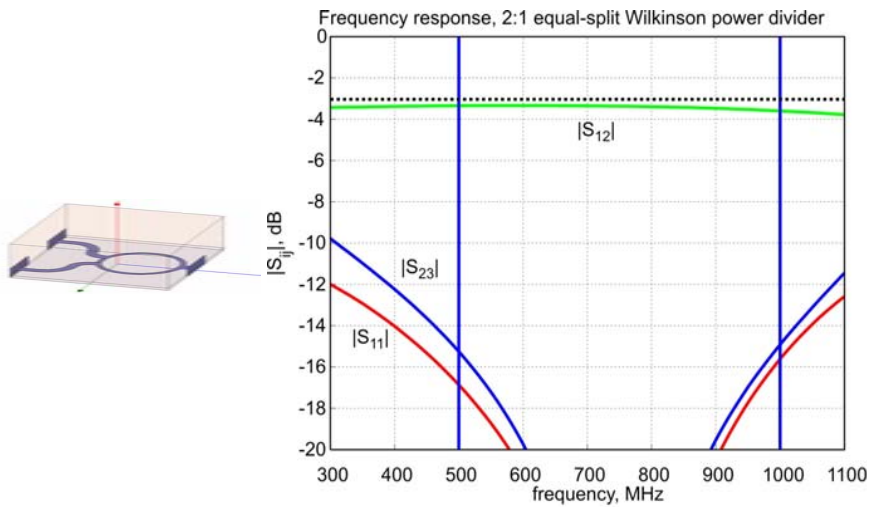
- **Return Loss for an infinite antenna array of ribcages with tapered balun**



- **1.92 x 1.92 m (8x8) array**
- **Equivalent to a 3 m parabolic reflector antenna**

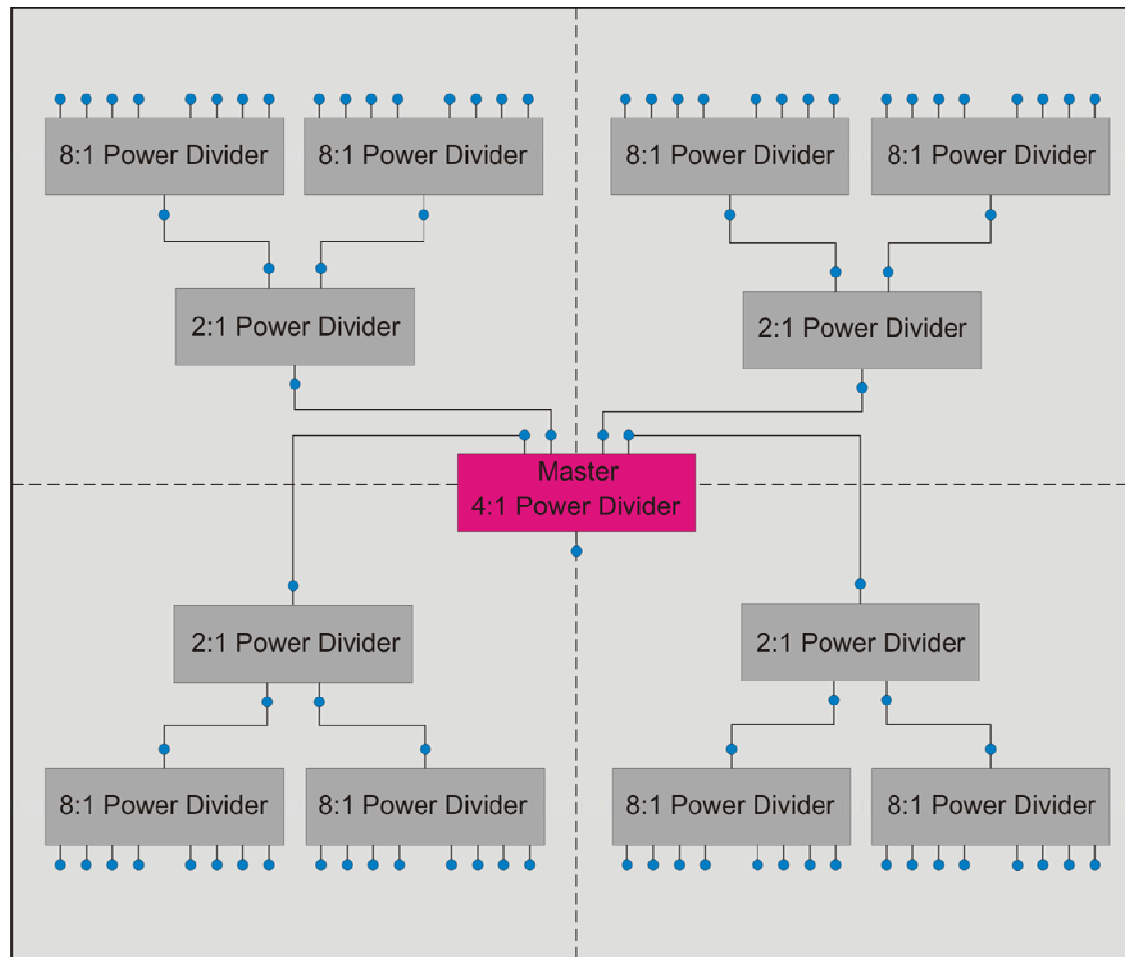
Optimized Power Dividers

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Feeding Network for 8x8 Array of Ribcages

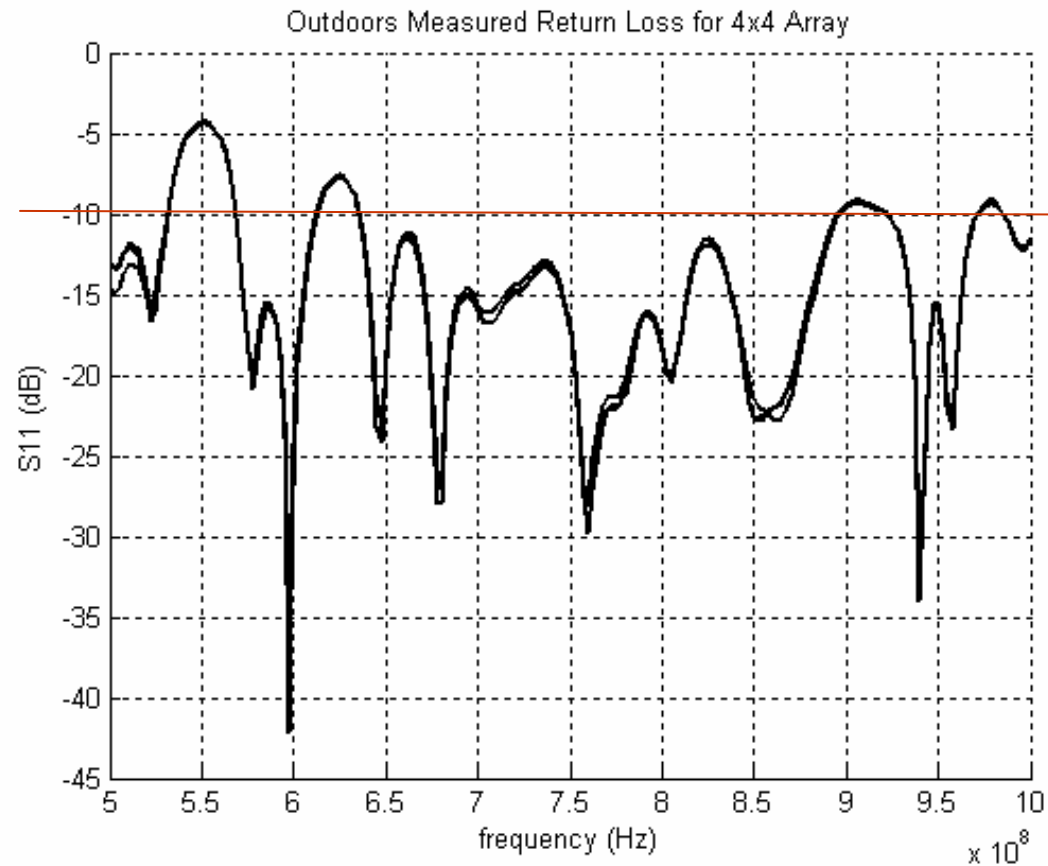


Measured Return Loss for the 4x4 Sub-Array Module

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- Replacement for conventional Digital TV antennas



- S_{11} for a 4x4 array of ribcage dipoles
- It can be used for Digital TV reception in the UHF band: 400-900 MHz



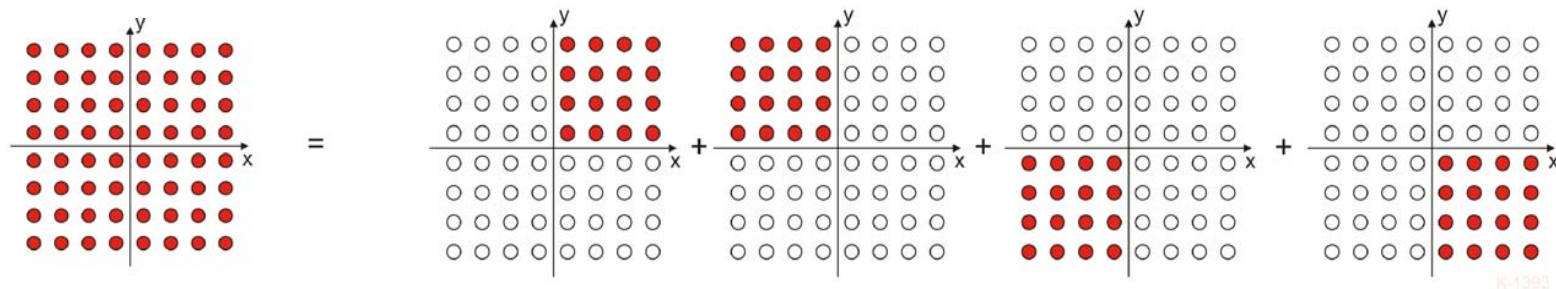
Simplified 8x8 Antenna Array Pattern Modeling

- Modeling a **finite 8x8 antenna array** of ribcage dipoles with balun in Ansoft HFSS requires
 - ~ 21 hours
 - 70 GB of memory on a
 - 64-bit Windows machine
- We have developed a simplified methodology that exploits the symmetry of the array and array excitations
- We have implemented an algorithm that allows to compute the total field pattern for the 8x8 antenna array from the analysis of one 6x6 sub-array
- Modeling a **finite 6x6 sub-array** of ribcage dipoles with balun in Ansoft HFSS requires
 - ~ 6 hours
 - 20 GB of memory on a
 - 64-bit Windows machine

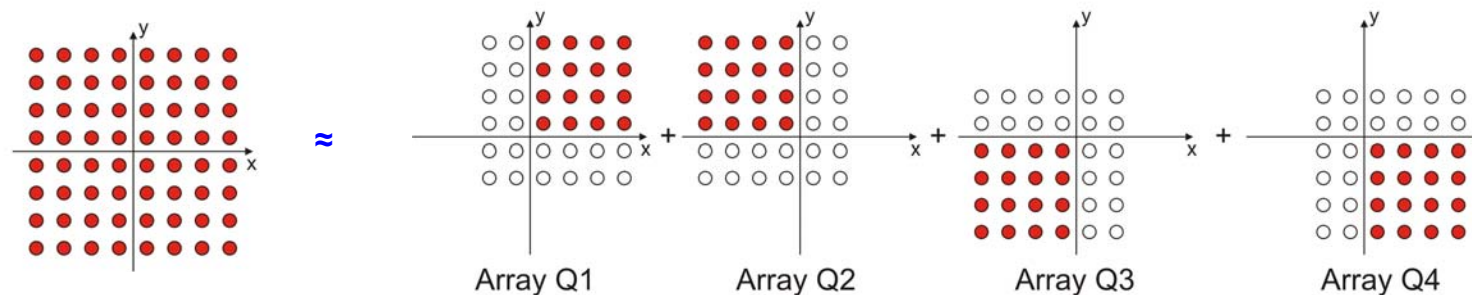
Simplified Composite Array Model

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- The total array field pattern can be expressed as superposition of four array field patterns, when the quadrants Q1, Q2, Q3, and Q4 are excited
- Only 16 elements are excited at any one time, while the remaining elements are passive and match-terminated ($50\ \Omega$)



- Approximation: truncate the passive arrays by removing the two outermost rows and columns.
- Now there are four 6x6 arrays, which can be analyzed/simulated separately



- When the array excitation is symmetric with respect to the x- and y-axes:

$$\bar{E}_{Q3}(\theta, \varphi) = -\bar{E}_{Q1}(\theta, \varphi)$$

- Q2 and Q4 are mirror images of Q1 and Q2:

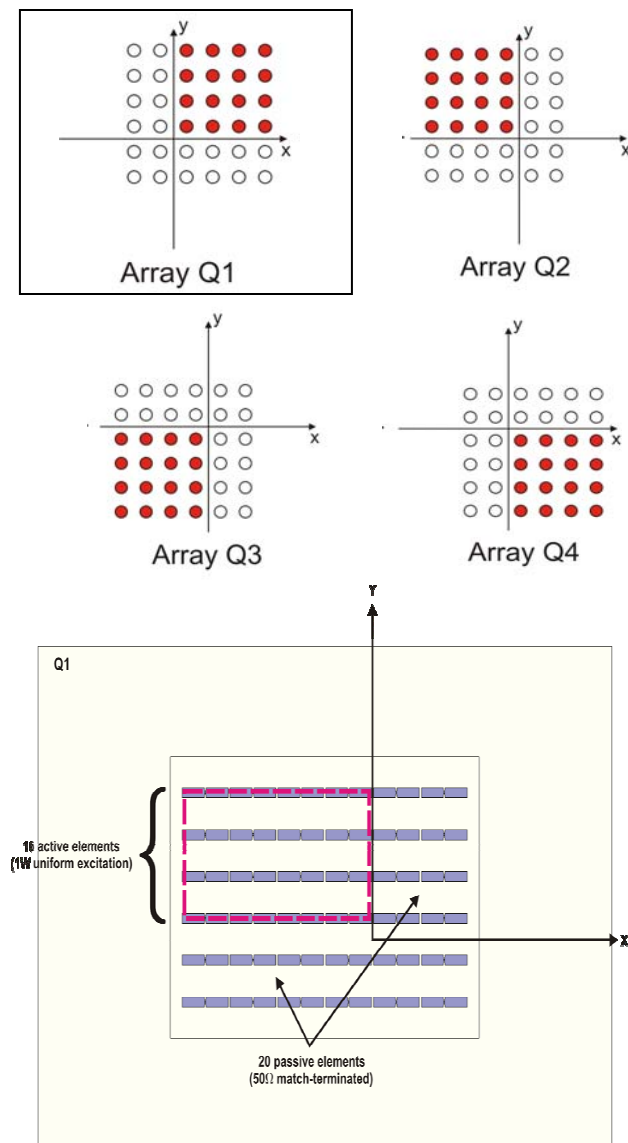
$$\bar{E}_{Q2,\theta}(\theta, \varphi) = -\bar{E}_{Q1,\theta}(\theta, \pi - \varphi)$$

$$\bar{E}_{Q2,\varphi}(\theta, \varphi) = \bar{E}_{Q1,\varphi}(\theta, \pi - \varphi)$$

$$\bar{E}_{Q4,\theta}(\theta, \varphi) = \bar{E}_{Q1,\theta}(\theta, -\varphi)$$

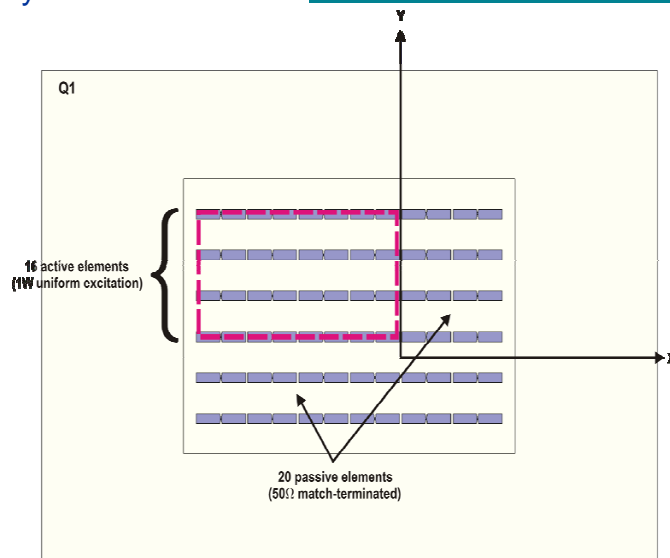
$$\bar{E}_{Q4,\varphi}(\theta, \varphi) = -\bar{E}_{Q1,\varphi}(\theta, -\varphi)$$

- A highly accurate representation for the far field of the 8x8 array can be obtained from the computation of a single 6x6 array (Q1)

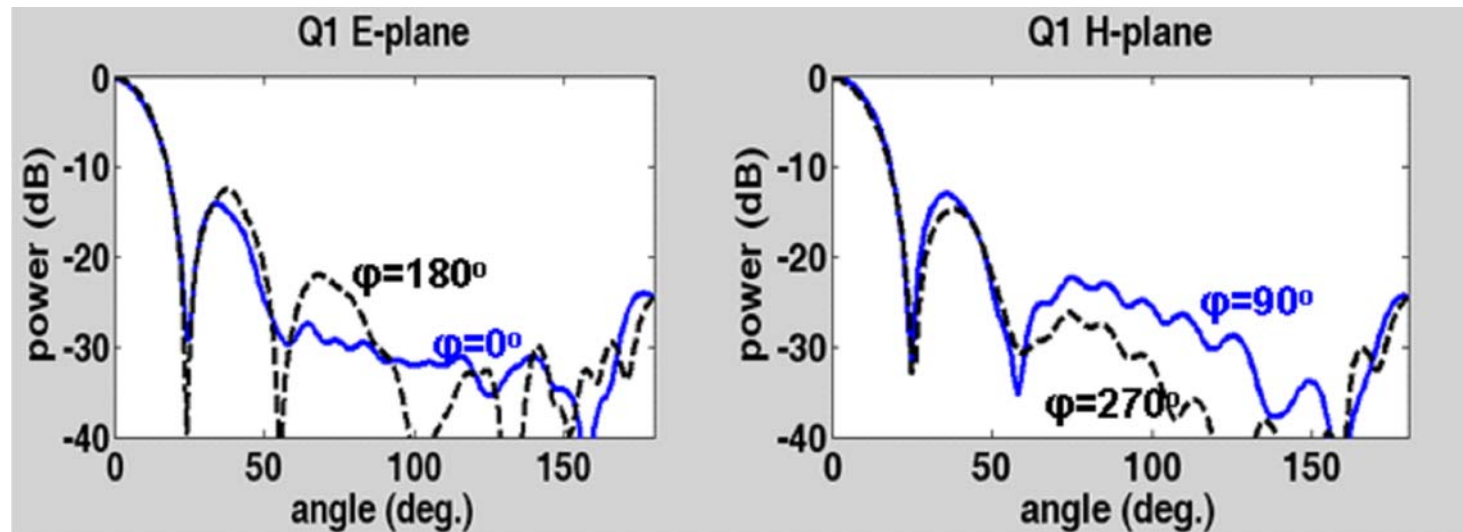


Q1 Sub-Array Pattern

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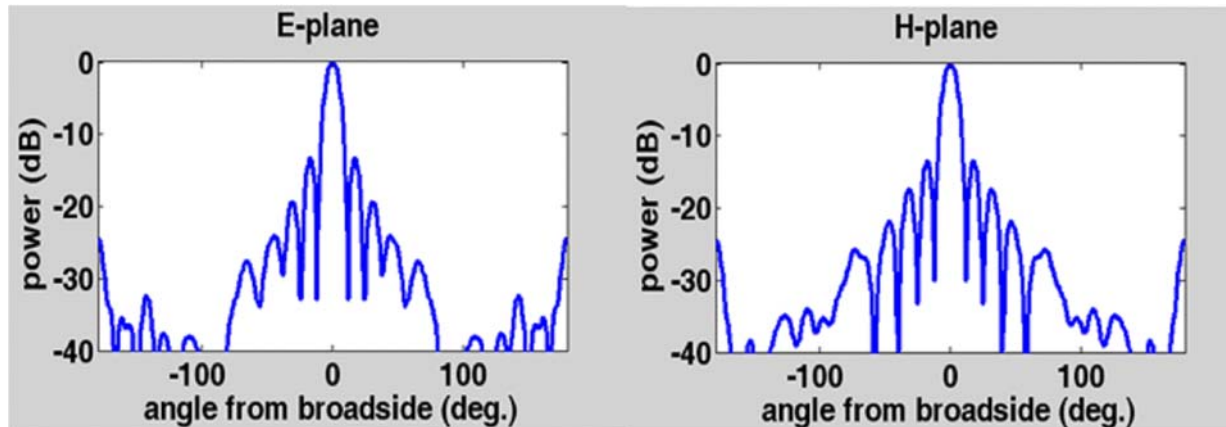
**Q1 sub-array pattern at 750 MHz:
E-plane and H-plane**



8x8 array Gain From Simplified Composite Array Model

The array directivity D is obtained by simple integration:

$$D = \frac{|E_{\max}|^2}{\iint |E_{\max}|^2 \sin \theta d\theta d\phi}$$



Frequency	Aperture Gain	Gain Computed from Composite Array Model	Total Gain (array gain - net loss in feeding network)
500 MHz	21.1 dB	21.5 dB	19.0 dB
750 MHz	24.6 dB	24.7 dB	22.2 dB
1000 MHz	27.1 dB	26.4 dB	23.9 dB

Conclusions

- **Wideband ribcage dipole as a single radiator:**
 - Combines advantages of blade dipole and droopy dipole
 - Achieves wide impedance bandwidth up to 3.2:1 while maintaining good pattern stability
 - Has low profile when mounted parallel to a ground or air vehicle

- **Array of ribcage elements:**
 - Has performance similar to a parabolic antenna while occupying less volume (e.g. 3 m diameter vs 1.92x1.92 m)
 - Can be stowed and transported in smaller sub-array modules (e.g. four 4x4 sub-arrays for an 8x8 array)
 - Its gain pattern was computed using a Simplified Composite Array Model

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